



PATENT SPECIFICATION

802,483

Date of Application and filing Complete

Specification: April 15, 1955.

No. 10891/55.

Application made in United States of America on April 23, 1954.

Complete Specification Published: Oct. 8, 1958.

Index at acceptance:—Classes 41, B(2A:17); 82(2), M; and 83(4), S(2G:4).

International Classification:—B01k, B23k.

COMPLETE SPECIFICATION

Improvements in or relating to Method of Dip Brazing Aluminous Metal

We, ALUMINUM COMPANY OF AMERICA, a corporation organised under the laws of the State of Pennsylvania, United States of America, of Alcoa Building, Pittsburgh, Pennsylvania, United States of America, do hereby declare the invention, for which we pray that a patent may be granted to us, and the method by which it is to be performed, to be particularly described in and by the following statement:—

This invention relates to the dip-brazing of aluminous metal, in which assemblies of aluminous metal members and filler metal in brazeable relationship are brazed by immersion in a molten salt bath. As used herein, the phrase "aluminous metal" includes aluminum of various grades (i.e. various grades of purity of aluminium) and aluminum base alloys.

20 In dip-brazing aluminous metal, the members to be joined are assembled in the desired structural relationship to each other with a suitable filler metal provided at the joint or joints, and the assembly is immersed 25 in a molten salt bath maintained at a temperature above the liquidus of the filler metal but below the solidus of the structural members. The salt bath serves both to heat the assembly to the brazing temperature and promote the flow of filler metal. The salt baths used heretofore have contained active flux salts in sufficient amounts to cleanse the surfaces of the structural members so that they 30 may be "wetted" by the filler metal and to assist in the spread of the filler metal in the joint area. The base or major portion of such salt baths has generally consisted of two or more alkali metal chlorides, and the active flux portion has been composed of other halides, especially the fluorides of alkali metals and aluminum. In particular, lithium halides have been included in nearly all commercial brazing baths because they not only reduce the melting point of the salt mixtures 40 but they have a very desirable effect on the

flow of molten brazing alloy on the aluminous metal surface. Baths containing little or no lithium halides have been regarded as inferior and unreliable, yet lithium salts are relatively expensive and, at times, are difficult 50 to obtain.

One difficulty associated with the dip-brazing process has been the loss of bath components by decomposition of one or more of the components by hydrolysis or other reactions, 55 and an economic loss that is always suffered is that which occurs by reason of the drag-out of molten bath clinging to the brazed members when withdrawn from the bath. The decomposition is influenced by the amount of 60 water present in the bath and the nature of the components employed, some being more greatly affected by water than others. The presence of some water is unavoidable, it being introduced by fresh salt additions, by 65 the parts being brazed or merely by exposure of the salt bath to the atmosphere. Thus, even though a salt mixture might be completely anhydrous when first melted, it quickly picks up some moisture which reacts with 70 one or more of the salts. The reaction not only causes a loss of individual salts but creates an undesirable sludge that must be removed eventually. Obviously, the losses from decomposition and drag-out are of 75 greater economic importance where the flux contains relatively costly material, such as lithium-containing compounds. Up to the present time it has not been found possible to use, in the ordinary way, a dip-brazing bath 80 composed almost entirely of low cost halides because such baths either do not clean and flux the aluminous metal surface, have such a short life as to be of no practical value in plant operations, or are very sensitive to the 85 adverse effect of impurities.

It is an object of this invention to provide a method of dip-brazing aluminous metal in salt baths composed entirely or for the most part of salts which have little or no inher- 90

[Price]

ent fluxing action on the metal surface. Another object is to provide a method of activating a salt bath which is otherwise substantially devoid of ability to flux an aluminous surface. Still another object is to provide a method of dip-brazing aluminous metal in a salt bath activated by a new means but which permits use of the dip-brazing techniques of the prior art. A further object is to provide a method of dip-brazing in a bath which is substantially free from sludge formation resulting from hydrolysis of salt components, even though substantial amounts of readily hydrolyzable salt components are contained therein. Still another object is to provide a flux bath which contains a very small amount of lithium salts, or even none at all, and yet has a sufficient degree of activity for dip-brazing purposes.

According to the invention, there is provided a method of dip-brazing aluminous metal members, which comprises successively immersing assemblies of said members and filler metal in brazeable relationship in a molten salt bath containing as its essential components by weight 2 to 70% total of at least one of beryllium chloride, magnesium chloride, calcium chloride, strontium chloride and barium chloride and 30 to 80% total of at least one of sodium chloride and potassium chloride, the total amount of all of said chlorides constituting the major portion of said salt bath, and activating said salt bath by at least periodically passing a direct electric current through the bath, the magnitude and duration of the current flow being adjusted to liberate nascent chlorine in the bath.

We have found that nascent chlorine liberated in the bath effectively activates the bath, whereas bubbling chlorine gas through the bath is ineffective for this purpose. Only a very small direct current is necessary to activate the bath. Salt baths according to the invention that contain little or no lithium salts, when treated in this manner, have been found to possess, in a high degree, the characteristics of prior art flux baths, which included large amounts of lithium compounds. In addition, it has been found that such baths activated in this manner inhibit sludge formation arising from hydrolysis of salt components. The nascent chlorine need not be liberated at or near the surface of the aluminous metal being brazed, so long as it is generated within the bath by electrolysis. It is dissolved, sorbed or otherwise held by the fused salt and appears to establish what we believe to be a non-oxidizing condition as opposed to an oxidizing condition. An oxidizing condition is considered to exist when the surface of the aluminous metal parts become coated with an oxide film which prevents brazing.

The salt bath, should have as its essential components from 2 to 70% total by weight

of at least one of beryllium chloride, magnesium chloride, calcium chloride, strontium chloride and barium chloride, these being hydrolyzable chlorides, and from 30 to 80% total of at least one of sodium chloride and potassium chloride, these being the common alkali metal chlorides, the total amount of all of the hydrolyzable and common alkali metal chlorides constituting the major portion of the bath.

To obtain the desired characteristics in the bath it is necessary, as mentioned above, to include at least one salt of the group consisting of beryllium chloride, magnesium chloride, calcium chloride, strontium chloride and barium chloride. These salts hydrolyze in contact with minute amounts of water present in the bath and probably tend to form an oxide or an oxyhalide or perhaps some other oxygen-containing products. Formation of such products is inhibited by the small amount of nascent chloride generated in the bath by passing a direct current therethrough. The precise manner in which these chlorides function and the part the products of hydrolysis play in the flux are not clearly understood, but it has been ascertained that at least one of these chlorides is essential in salt fluxes activated in accordance with the invention. The proportion of hydrolyzable chloride to be used will vary with the number selected and with the alkali metal chloride with which it is associated, and it is desirable that the total amount of hydrolyzable chloride be within the range of 20 to 70% of the weight of the flux bath. Calcium chloride is a cheap and otherwise suitable hydrolyzable chloride to use, and especially where other components than calcium chloride and alkali metal chloride are used it is preferable to employ it in a range from 20 to 40%. Where strontium chloride is employed, it is preferable to employ it in a range of 2 to 15%. Where one or more of the remaining hydrolyzable chlorides is used, from 10 to 30% total is preferred. Strontium chloride has the special effect of promoting flow of the fused filler metal between the metal members being brazed and hence it is frequently desirable to include a small amount of this salt in the flux, especially if no lithium chloride is employed.

The alkali metal chloride portion of the bath should be selected with a view to the melting point of the salt mixture. Sodium chloride and potassium chloride are considered to be neutral components inasmuch as they have no fluxing action, but both may be used in providing a relatively low melting point bath. Lithium chloride, while not specifically essential, may be used along with the common alkali metal chlorides since it definitely improves the flow of fused filler metal when used in a salt bath activated in accordance with the invention. Although

amounts up to as much as 25% may be used effectively, we have found that very satisfactory bath compositions can be formulated for activation in accordance with the invention which contain from 0.2 to 5% of this chloride, and preferably less than 2%. The common alkali metal chloride may be employed in amounts such that the total is preferably within the range of 50 to 80% when more than one is used. In our preferred compositions the portion of the bath composed of both the hydrolyzable and alkali metal chlorides preferably constitutes at least 90% of the entire composition. Of all the alkali metal chlorides those of sodium and potassium are preferred, and for purposes of this invention are regarded as constituting a group of related salts.

Along with the salts so far mentioned, the bath may also, and preferably does, contain from 0.5 to 10% total of at least one salt of the group beryllium fluoride, magnesium fluoride and aluminum fluoride and the double fluorides of aluminum and the alkali metals. The double fluorides of aluminum and sodium or potassium, for example, form the well-known substances known as cryolite and chiolite. If the double fluorides are not available, alkali metal fluoride and aluminum fluoride may be added to the bath in the proportions necessary to form a double fluoride. From the standpoint of cost, aluminum fluoride or the double aluminum fluorides are preferred as bath components of this group. All of the foregoing fluorides have a beneficial action in preparing the aluminous metal surface for brazing and in their absence the action of the bath is slower. They also appear to undergo some degree of hydrolysis as do the chlorides of the group mentioned above and with similar advantages to the performance of the bath activated in accordance with the invention. In the preferred practice, the indicated fluoride is used in amounts of 2 to 5%.

In general the salt bath should have a liquidus no higher than 1100°F., in order to have a bath which possesses high fluidity and which will minimize drag-out. Ordinarily a melting point range of between 900 and 1100°F. will be found to be quite satisfactory.

The following are a few examples of lithium-free and low-lithium salt baths useful in accordance with the invention, the proportions being expressed in percentage by weight:

(1)	35 NaCl 65 CaCl ₂
(2)	15 NaCl 41 KCl 30 CaCl ₂ 6 SrCl ₂ 8 Na ₃ AlF ₆

60

65

(3)	0.5 LiCl 22 NaCl 46 KCl 29 CaCl ₂ 2.5 Na ₃ AlF ₆
-----	---

70

The molten salt baths described are all either inert from the standpoint of fluxing aluminous metal for brazing or, at best, only moderately active for short periods, until they are activated as by the procedure now to be described. We have found that brazing of aluminous metal may be periodically and repeatedly effected in a molten bath of the character described if it is activated as a flux by at least periodically passing direct current through the bath. The direct current may be caused to flow at intervals or continuously, its magnitude and duration being adjusted to liberate nascent chlorine in the bath as the activating agent.

85 A convenient method of introducing the current is to connect a small direct current source to two aluminum electrodes immersed in the bath, but electrodes made of other material not introducing harmful impurities may also be employed. It is preferable to keep the anode current density in the range between 0.05 and 1 ampere per square inch, but higher current densities may be employed. We have found a current of a magnitude at least of 0.01 ampere per pound of bath to be desirable, but it is usually not necessary to employ a current greater than 0.1 ampere per pound, nor to maintain the current continuously. In fact, current flow during 1/2 to 2 hours per day has been found sufficient where a bath was being used 8 hours per day.

95 In a particular form of the invention, the aluminous metal of the assemblies being brazed is made the anode in the salt bath. In this case it is especially desirable to employ a low anode current density, e.g., of 0.05 to 1 ampere per square inch of aluminous metal surface, and preferably about 0.25 ampere per square inch. Making the work the anode is very effective since the nascent chlorine from electrolysis is generated right at the surfaces to be brazed, and the aluminum oxide film on such surfaces is readily, removed. This form of the invention is, however, sometimes objectionable because of a tendency to etch the aluminous surfaces exposed outside the joint or joints, although the etched conditions can be eliminated quite simply by subsequent surface treatments that may be required in any event. A further observation concerning this form of the invention is that a "foam" sometimes builds up on the parts being brazed. This condition can readily be minimized by shutting off the current prior to removal of the assembly from the bath, and the foam can be eliminated by a mere momentary reversal of the current.

130

In addition to activating the salt bath as a flux, the introduction of a direct current has additional advantages. It electrolyzes any water in the bath and plates out any heavy metal impurities. Therefore, less care need be taken to avoid slight water contamination or the introduction of small amounts of heavy metal. However, the current flow must be continued so as to generate nascent chlorine in the bath in order to activate, as an aluminous metal flux, a bath not otherwise having flux properties.

The procedures so far described may advantageously be used in connection with 15 baths according to the invention treated to some extent by the procedures described in our Application No. 22,858/53 Serial No. 744,862, wherein the salt bath is treated with at least one anhydrous hydrohalide of the 20 group consisting of hydrogen fluoride and hydrogen chloride, these being gaseous at the salt bath temperature and ordinary pressure and providing hydrohalide in the bath. When a direct current is employed to activate a 25 hydrohalide-treated bath, the extent of the hydrohalide treatment and the magnitude and duration of the current flow may be adjusted so that either treatment, or both, may be less rigorous or prolonged. In other 30 words baths treated with hydrohalide either to an extent insufficient to activate the same, or which fail to maintain their activity through use or otherwise, are readily amenable to activation by the direct current treatment described herein.

The direct current activation may be applied to a bath previously treated with hydrohalide or it may be effected conjointly with the introduction of hydrohalide if desired. Direct current activation of a hydrohalide-treated bath is especially effective for producing satisfactory brazing response over extended periods of time at low cost. The hydrohalide treatment may consist in 45 periodically introducing hydrohalide in a small amount up to that required to saturate the molten salt bath. By "saturation" we mean the maximum capacity of the fused salt for holding the hydrohalide, both chemically and physically. At present there is no known means of ascertaining the actual amount of hydrohalide short of saturation, which is present at any given time.

As indicated hereinabove, the hydrohalides which may be used are anhydrous hydrogen chloride and hydrogen fluoride. The other hydrohalides, hydrogen iodide and hydrogen bromide, probably decompose at the temperature of the fused salt, but in any event, they are ineffective in preparing the salt baths for brazing purposes. Of the two useful hydrohalides, hydrogen chloride is preferred because of its low cost and because it gives rise to very little fume. It is essential, in any case, to use the dry gas to avoid

an excess of water in the flux. Although the two anhydrous hydrohalides may be used separately, it may be advantageous to use them jointly. Furthermore, it is possible to dilute the hydrohalide with a suitable inert 70 gas such as helium, argon and even nitrogen.

In general, it may be desirable to introduce a small amount of gaseous hydrohalide regularly, for example, for a half hour or so per day. A period of time is necessary to 75 allow the gas to permeate the liquid salt and aid in establishing the non-oxidizing condition required for brazing. A slow rate of introduction has been found to be most suitable. Whenever the desired hydrohalide 80 treatment condition has been achieved, a lower flow rate can be used or none at all. In general, an initial flow of 0.02 to 1.0 cc. per minute at 14.7 p.s.i. absolute pressure and 70°F. of anhydrous hydrohalide gas per 85 pound of flux is recommended. The flow rate and period of treatment in any given case will, of course, vary with the extent of the direct current treatment, the size of the bath being treated, and the utilization of the 90 bath for brazing.

Anhydrous hydrohalide may be introduced into the molten salt bath in any suitable manner either from a source of compressed gas or from a gas generator. The gas may 95 be passed into a perforated pipe or a porous cup held near the bottom of the bath and allowed to slowly bubble through the salt bath. Other known means of contacting a liquid with a gas may be employed if adapted 100 to operate in a fused salt environment. A perforated pipe or porous cup has the advantage of dividing the gas into small streams of bubbles and thereby obtaining better contact between the gas and the salt. Also, 105 such a gas distributing means can be readily removed from the fused salt bath when desired. Instead of introducing the hydrohalide gas from an external source, it is possible to use decomposable halides which 110 yield no undesirable residue. Such substances as ammonium chloride may be employed.

The customary procedures followed in dipping brazing with conventional flux baths can be 115 used in employing the salt bath, treated in accordance with the invention. That is, substantially the same bath temperature ranges and periods of immersion may be employed as have been utilized in prior practice 120 for brazing the same type of article. To secure the best results, however, it is preferable to use slightly higher temperatures than might normally be employed. The employment of the same procedures is of considerable practical advantage, for it means 125 that our activated salt bath can be substituted for conventional baths without altering the plant practice to any significant extent.

The aluminous metal to be brazed may be 130

of any shape or size which will permit assembly and immersion in the salt bath. The filler metal may be provided in the form of wire, strip or stampings which are placed 5 at the location of the joints prior to brazing, or it may be supplied as a coating on a sheet as shown in British Patent 539,337 or as an intermediate layer in a composite sheet product such as illustrated in United States 10 Patent 2,602,413. The composite sheet products having a coating or intermediate layer of brazing alloy are commercially referred to as brazing sheets. This material is very well adapted to the production of brazed 15 articles and has been found to be especially suited to the production of dip brazed products.

The filler or brazing alloy may be any one of the commonly used compositions. Aluminum-silicon alloys containing from 2 to 12% silicon are very satisfactory as well as those aluminum-silicon type alloys which contain from 2 to 5% copper and/or 7 to 12% zinc. The choice of brazing alloy will be determined, in part, by the temperature at which 25 brazing is done; in general, those alloys having the largest amounts of added elements being useful at lower brazing temperatures than those compositions having a smaller 30 amount of added components.

In order to insure operation of the salt bath at its highest efficiency if the bath is not initially electrolyzed, it is ordinarily necessary to purify the molten mixture prior to 35 dip-brazing by suspending pieces of aluminum in the bath for a period of time. In commercial operations, this is usually done by suspending coils of aluminum wire or strip in the bath for a number of hours during 40 the period of melting and bringing the bath up to brazing temperature. If the bath remains idle for some time, even though in molten condition, it has sometimes been necessary to repeat the treatment with aluminum before brazing is attempted. The treatment appears to remove excess water and metallic impurities which may be associated with the salts or derived from the container or heating elements submerged in the bath. 45 However, with the use of a direct current in accordance with the invention, the above-described dehydrating step may be eliminated, if desired, as the current electrolyzes the water content of the bath. The hydrohalide 50 treatment is also effective in removing water by entrainment, but is most effective for actually reversing decomposition by hydrolysis and thus keeping the bath acid.

As an example of a particular form of the 60 invention described, T joints between members of an aluminum alloy containing 1.2% manganese, employing shims of an aluminum brazing alloy containing 10% silicon as filler metal, were made in bath (1) identified 65 above, by immersing the assemblies and mak-

ing them the anode in the bath at a current density of 0.16 ampere per square inch for 4 minutes at 1100°F. The current flow per pound of bath was approximately 0.08 ampere. 70

As an example of another form of the invention, double T joints between two pieces of aluminum alloy containing 1.2% manganese and one piece of aluminum brazing sheet having on one side thereof a coating of 75 aluminum brazing alloy containing 5% silicon providing filler metal, were brazed in bath (3) identified above, by immersing the assemblies in a previously electrolyzed bath for a few minutes at 1100°F. Separate 80 aluminum alloy electrodes were employed to introduce a continuous current of approximately 0.25 ampere per square inch of electrode surface. The current flow per pound of bath was approximately 0.01 ampere. 85

As an example of the form of the invention in which the direct current is applied to a hydrohalide-treated bath, numerous aluminous metal assemblies, similar to those of the other examples, were brazed, from day 90 to day throughout an 8 hour shift, in bath (3) identified above, by immersing the assemblies in the bath for a few minutes at about 1100°F. The bath was treated daily for about one-half hour with hydrogen chloride 95 at the rate of about 1 cc. per minute per pound of bath. Separate aluminum electrodes were employed to introduce a current of approximately 0.5 ampere per square inch of electrode surface. The current flow per 100 pound of bath was approximately 0.05 ampere. However, the current was employed for only an hour or two each day.

WHAT WE CLAIM IS:—

1. A method of dip-brazing aluminous metal members, which comprises successively immersing assemblies of said members and filler metal in brazeable relationship in a molten salt bath containing as its essential components by weight 2 to 70% total of at least one of beryllium chloride, magnesium chloride, calcium chloride, strontium chloride and barium chloride, and 30 to 80% total of at least one of sodium chloride and potassium chloride, the total amount of all 110 of said chlorides constituting the major portion of said salt bath, and activating said salt bath by at least periodically passing a direct electric current through the bath, the magnitude and duration of the current flow 115 being adjusted to liberate nascent chlorine in the bath.

2. A method according to Claim 1, in which the total amount of the first group of chlorides is between 20 and 70%. 125

3. A method according to Claim 1, in which said salt bath contains 20 to 40% of calcium chloride or 2 to 15% of strontium chloride or 10 to 30% total of at least one of beryllium chloride, magnesium chloride, and 130

barium chloride and 50 to 80% total of sodium chloride and potassium chloride.

4. A method according to any of Claims 1 to 3, in which said salt bath also contains 5 0.2 to 5% of lithium chloride.

5. A method according to any of Claims 1 to 3, in which the total amount of all of said chlorides constitute at least 90% of said salt bath.

10 6. A method according to any of Claims 1 to 5, in which said salt bath also contains 0.5 to 10% of at least one salt of the group beryllium fluoride, magnesium fluoride, and aluminum fluoride and the alkali metal-
15 aluminum double fluorides.

7. A method according to any of Claims 1 to 6, in which the current flow is at least 0.01 ampere per pound of salt bath.

8. A method according to any of Claims 1

to 6, in which the assemblies are made the 20 anode in the salt bath, and the current density is maintained between 0.05 to 1 ampere per square inch of aluminous metal surface.

9. A method according to any of Claims 1 to 8, which includes treating the salt bath with at least one anhydrous hydrohalide of the group consisting of hydrogen fluoride and hydrogen chloride.

10. A method of dip-brazing aluminous 30 metal members substantially as hereinbefore described.

11. Brazed aluminous metal members whenever prepared by the method according to any of Claims 1 to 10.

STEVENS, LANGNER, PARRY &
ROLLINSON,
Chartered Patent Agents,
Agents for the Applicants.

Printed for Her Majesty's Stationery Office by Wickes & Andrews, Ltd., E.C.4. 684/2.—1958.
Published at The Patent Office, 25, Southampton Buildings, London, W.C.2, from which copies
may be obtained.